

# INFLUENCE OF STRONGER OVERLYING LAYER AND REINFORCEMENT ON CBR PROPERTY OF DIFFERENT SOFT SUBGRADE - A LAB STUDY

## DIFFERENT SOFT SUBGRADE

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**Abstract:** Utilization of bulk quantities of natural soil is a viable technique in pavement constructions. Natural Subgrade supports the pavement loads and hence should have adequate strength. Providing stronger layer above soft layer and reinforcing weaker soils using geo-synthetics like geo-grids are few techniques to improve subgrade performance. Present project work aims to study the influence of stronger aggregate layer over soft soil subgrade with and without reinforcement at the interface over CBR property of different subgrade. Four subgrade types with varying plasticity properties are used for present study. Laboratory and field CBR tests are conducted with varying  $H_r$  ( $H_a / H_s$ ) from 0, 0.1, 0.2, 0.3, 0.4 0.5. Where  $H_s$  and  $H_a$  are thickness of subgrade and thickness of overlying aggregate respectively. Effect of separator reinforcement (geosynthetic) is also studied on CBR for various  $H_r$ .

**Index Terms:** Plasticity index, CBR value, reinforcement, subgrade, stronger overlying layer, and Geosynthetics

### I. INTRODUCTION

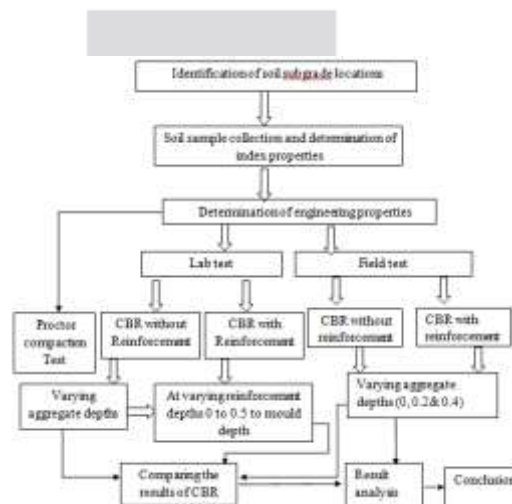
The service-life and performance of roads depend to a large extent on the strength and stiffness characteristics of subgrade. Subgrade characteristics assist road engineers in the selection of materials for sub-base and base courses of pavements. Hence, the evaluation of subgrade strength assumes great importance in pavement design. In geotechnical and foundation engineering, in-situ penetration tests have been widely used for site investigation in design. California Bearing Ratio (CBR) value is very popular among highway engineers as a soil support value for pavement design.

Geosynthetics have been used for subgrade stabilization and base course reinforcement for construction of unpaved structures. Placed between the subgrade and the base course, or within the base course, the Geosynthetic improves the performance of the unpaved roads carrying channelized traffic and unpaved areas subjected to random traffic. Geosynthetics in road structures can have a reinforcement, separation and filtration function. Because of the reinforcement function significant higher shear stresses can be observed at the interface subbase - geosynthetic - subsoil.

#### Objective

- To determine the laboratory CBR and engineering properties for a four soil subgrades viz., clayey soil of varying plasticity characteristics.
- To study the influence of stronger aggregate layer over soft soil subgrade with / without separator reinforcement at the interface over composite CBR property of soil- aggregate subgrade.
- To study the influence of fines content, plasticity and varied thickness of overlying stiff aggregate layer with and without NIPM separator reinforcement on CBR value of composite subgrades.

### II. METHODOLOGY



### III. EXPERIMENTAL STUDIES

Experimental studies for determination of index and engineering properties on different subgrade are carried out. The engineering properties are determined on subgrade samples in both lab and field. Four types of soil subgrade, Geotextile reinforcement and coarse aggregate are used for study.

#### Preparation of aggregate-geotextile-soil specimen and conduct of lab California Bearing Ratio(CBR) Test:

Lab CBR test is carried out on soil-aggregate composite layer of thickness, H by placing aggregate layer of thickness,  $H_a$  over soil layer of thickness,  $H_s$  in CBR mould. Initially soil layer is compacted in the mould to maintain  $H_s$ , aggregate of thickness  $H_a$  is later filled in the mould above soil. The testing is carried out by varying  $H_r$  (a ratio of  $H_a$  to  $H_s$ ). The same tests are carried out by placing a separator geotextile at the interface of soil-aggregate. The thickness of sample H and the densities of soil and aggregate is maintained throughout all the tests. For creating void of height  $H_a$  spacer disks of thickness 0.5, 1cm, 2cm etc. are used for preparing soil specimen with the desired void space (later filled by coarse aggregate) above soil after compaction in CBR mould. A schematic diagram of lab CBR sample specimen is given in fig.3.2. The samples are compacted at maximum dry density condition for performing CBR test and  $H_r$  is varied from 0 to 0.5 in the increments of 0.1. Test setup for sample without and with separator geotextile.

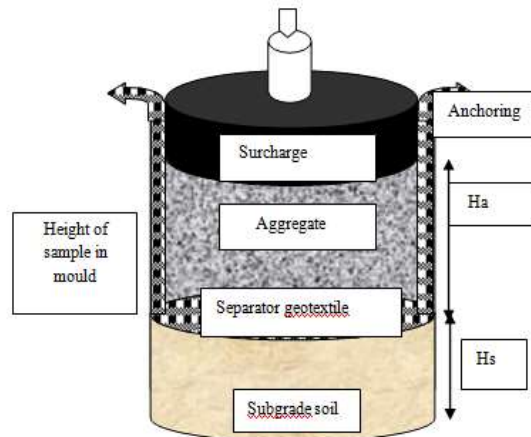


Fig-1: Schematic diagram of soil- aggregate- separator geotextile layers for lab CBR test

#### Preparation of aggregate-geotextile-soil specimen and conduct of field California Bearing Ratio(CBR) Test:

Field CBR is test conducted at subgrade from where sample-4 is collected. The test is conducted at a depth of 0.6m below ground. Initially a pit of size 1.5m x 1.0m is made. CBR test is conducted at different locations in the pit by varying  $H_r$ . For simplicity zone of influence of soil is taken to be same as thickness in lab. Accordingly  $H_r$  is computed and maintained in all the tests. The test set up is shown in figure-2.

Table 3: Engineering properties of Soil subgrade

Sample No.	$w_{max}$ (%)	$\gamma_d$ (kN/m <sup>3</sup> )	CBR (%)
1	17.07	16.90	2.07
2	18.97	16.18	1.66
3	21.04	15.94	1.20
4	15.40	18.14	2.76

Table 4: Lab and field density of subgrade-4

Lab Density(kN/m <sup>3</sup> )	Field Density(kN/m <sup>3</sup> )
18.14	18.75

**Table 5: CBR Ratios  $R_c$  and  $R_c^*$  obtained for soil subgrades#**

Parameter $H_r$	$R_{c1}$	$R_{c1}^*$	$R_{c2}$	$R_{c2}^*$	$R_{c3}$	$R_{c3}^*$	$R_{c4}$	$R_{c4}^*$
0	1	1.304	1	1.5	1	1.841	1	1.23
0.1	1.277	1.603	1.162	1.807	1.383	2.25	1.33	1.47
0.2	1.594	1.835	1.331	2.162	1.608	2.766	1.49	1.68
0.3	1.69	2.004	1.746	2.334	2.075	2.991	1.68	1.9
0.4	2.004	2.14	2.334	2.5	2.916	3.23	1.9	1.98
0.5	1.872	2.27	2.1	2.668	2.775	3.458	1.79	2.12

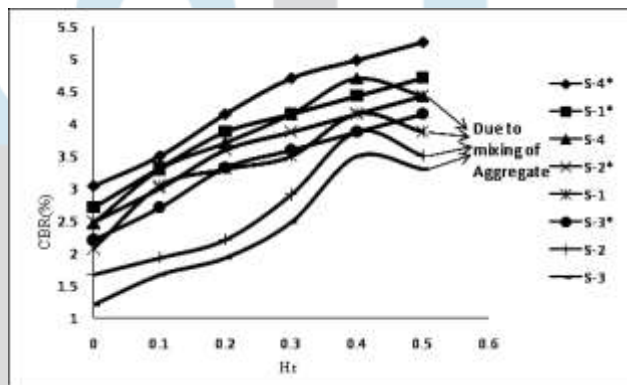
# subscript 1, 2,3,4 in table 5 indicates subgrade sample number.

**Table 6 CBR Ratios  $F_c, F_c^*$  and  $F_c^{**}$  obtained for soil subgrade**

$H_r$	Lab CBR value		Field CBR value		$F_c$	$F_c^*$	$F_c^{**}$
	$C_{ws}$	$C_s$	$FC_{ws}$	$FC_s$			
0	2.47	3.045	3.01	3.89	0.82	1.01	1.29
0.2	3.7	4.15	4.76	6.01	1.22	1.37	1.99
0.4	4.7	4.9	6.2	7.06	1.56	1.62	2.34

**Variation of CBR results with  $H_r$  : effect of separator**

The variation in CBR values with  $H_r$  of separator and without separator soil is shown in figure 4.65 it is observed that the CBR value is increasing with  $H_r$ . Using the separator is causing in increase of CBR value. Due to overlaying aggregate, the bearing resistance is increased. With increased  $H_r$  due to increased bearing resistance CBR value for all the three soils has increased considerably. With increase in value of  $H_r$  from 0 to 0.5 for three different samples, the corresponding CBR value has increased from 2.09 to 3.59; 1.66 to 3.5, and 1.2 to 3.3 for  $H_r$  ranging from 0 to 0.5 for without separator soil. There is also decrease in CBR value in spite of increasing the  $H_r$  value after a certain threshold level. This is due to lack of interlocking with the increase in air voids the resistance is affected. Similarly the CBR value has increased from 2.7 to 4.7; 2.49 to 4.43 and 2.21 to 4.15 for  $H_r$  ranging from 0 to 0.5 for separator soil. Here, the penetration of the aggregate is avoided by using separator.



**Fig 1: Variation of CBR with respect to  $H_r$**

**Presentation of variation of CBR Ratio  $R_c$  &  $R_c^*$  with  $H_r$ :**

The factored CBR values  $R_c$  and  $R_c^*$  and their variation with  $H_r$  is presented in Fig. 4.69. As expected and it can be seen that a significant contribution is achieved in CBR values due to aggregate and separator geotextile. Hence the problem due to low CBR of natural subgrade can be overcome by providing either overlying aggregate layer or separator or both. However the combination is to be chosen for best results. As observed from the graph for sample-3  $R_c^*$  has increased from 2.25 to peak value of 3.5 for  $H_r$  from 0 to 0.5, but  $R_c$  has increased only from 1.2 to a peak value of 2.75 for  $H_r$  from 0 to 0.4, and later decreased. The same trend is seen for other soil samples also.

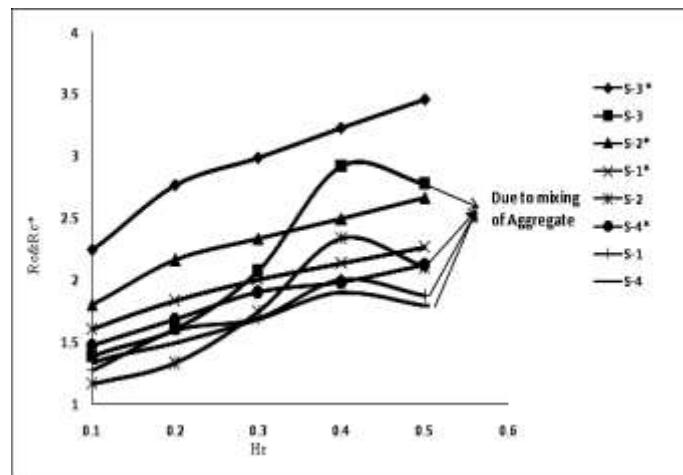


Fig 2: variation  $R_c$  &  $R_c^*$  with  $H_r$

#### IV. CONCLUSIONS

- Fines (%) and PI has an influence on CBR and it is observed that the CBR value decreased by 12% with respect to Fines (%) and by 11.72% with respect to PI.
- It is observed that the CBR value of composite soil (soil+ aggregate) is 33% more than that of soil alone.
- CBR of composite soil with separator soil ( $H_r=0.1$  to  $0.5$ ) are 23.47% and 50% higher than that of CBR values of the soil without separator.
- The effect of separator is insignificant at higher  $H_r$  value say 0.4 irrespectively of plasticity. The improvement is significant at low  $H_r$  of 0.2 over  $H_r$  0.4.
- Given a soil of plasticity index, the factored CBR, has provided a guideline for choosing optimum combination of aggregate and separator geotextile for a desired improvement by avoiding mixing.
- It is observed that the influence of separator reinforcement and aggregate is more in lab that of field.

#### REFERENCES

- [1] AGGARWAL.P, BAJINDER SHARMA (2011) "APPLICATION OF JUTE FIBER IN THE IMPROVEMENT OF SUBGRADE CHARACTERISTICS, ACEEE INT. J. ON TRANSPORTATION AND URBAN DEVELOPMENT", VOL. 01, NO. 01.
- [2] ASHA M. N., MADHAVI LATHA.G (2009)," BEARING RESISTANCE OF GEOSYNTHETIC REINFORCED SOIL-AGGREGATE SYSTEM, INDIAN GEOTECHNICAL CONFERENCE", PG.NO.185 TO 188.
- [3] ASHA, M.N., MADHAVI LATHA.G (2010) "MODIFIED CBR TESTS ON GEOSYNTHETIC REINFORCED SOIL- AGGREGATE SYSTEMS, INDIAN GEOTECHNICAL CONFERENCE", PG. NO.297 TO 300.
- [4] BANDYOPADHYAY. K., BHATTACHARJEE. S. (2010) "COMPARATIVE STUDY BETWEEN LABORATORY AND FIELD CBR BY DCP AND IS METHOD, INDIAN GEOTECHNICAL CONFERENCE", PG. NO. 1011 TO 1014.
- [5] CHEGENIZADEH.A, HAMID.N (2011), "CBR TEST ON REINFORCED CLAYEY SAND, INTERNATIONAL CONFERENCE ON ENVIRONMENTAL AND CIVIL ENGINEERING "(ICECE 2011), BANGKOK, THAILAND: WASET